

PROPOSAL FOR HYDROGEOLOGIC STUDY

HINSDALE - SEXTON LANDFILL

F05-8702-059

FIL0041GA

ILD00060647

December 23, 1987

US EPA RECORDS CENTER REGION 5



486809

TABLE OF CONTENTS

<u>Section</u>		<u>Page</u>
1	INTRODUCTION.	1-1
	1.1 Justification for Drilling	1-1
	1.2 Objectives	1-1
2	BACKGROUND.	2-1
	2.1 Site Description/History	2-1
	2.2 Geography/Physiography	2-2
	2.3 Geology/Hydrogeology	2-2
3	PROCEDURES.	3-1
	3.1 Introduction	3-1
	3.2 Hydrogeologic Investigation.	3-1
	3.2.1 Geophysical Investigation	3-1
	3.2.2 Monitoring Well Installation.	3-5
	3.2.2.1 Borehole Placement and Sampling.	3-5
	3.2.2.2 Monitoring Well Construction	3-6
	3.3 Aquifer Testing.	3-8
	3.3.1 Physical Testing.	3-8
	3.3.2 Chemical Testing.	3-8
	3.4 Surface Soil/Sediment Sampling	3-8
	3.5 Surface Water Sampling	3-8

Table of Contents (Cont.)

<u>Appendix</u>	<u>Page</u>
A BORING LOGS	A-1

LIST OF ILLUSTRATIONS

<u>Figure</u>		<u>Page</u>
2-1	Site Location Map.	2-3
2-2	Bedrock Elevation Map.	2-4
2-3	Structure Contour of the Bedrock Surface	2-5
2-4	Isopach of the Confining Unit.	2-6
2-5	Water Level of the Glacial Drift Aquifer 1972-1974 . . .	2-8
2-6	Water Depth of the Silurian Dolomite Aquifer 1972. . . .	2-9
3-1	Well Location Map.	3-2
3-2	Geologic Cross-Section From A to A'.	3-3
3-3	Geophysical Survey Location.	3-4
3-4	Proposed Soil Sample Location Map.	3-9

1. INTRODUCTION

1.1 JUSTIFICATION FOR DRILLING

The United States Environmental Protection Agency (U.S. EPA) has authorized Ecology and Environment, Inc., Field Investigation Team (E & E - FIT) to reevaluate the Hinsdale-Sexton Landfill in the form of a hydrogeological investigation. The primary goal of this investigation is to accurately assess the site for the National Priorities List (NPL). The projected Hazardous Ranking System (HRS) score will increase to greater than 28.5 if source contaminants are detected in the groundwater via migration pathways. A hydrogeological investigation will provide documentation of the existing conditions for final NPL consideration.

1.2 OBJECTIVES

The primary goal of this investigation is to detect source contaminants and analyze the potential for migration of contaminants to the aquifer(s) of concern. The project will include:

- A monitoring well program designed to characterize the aquifer(s) of concern and to determine the hydraulic connection between aquifers;
- Collection of chemical data derived from soil boring, groundwater, soil, and surface water sampling used to confirm existing data and to provide a reliable database for satisfying HRS model requirements; and

- An assessment of the interaction between surface water drainage and groundwater pathways.

2. BACKGROUND

2.1 SITE DESCRIPTION/HISTORY

The Hinsdale-Sexton Landfill, operated by the John Sexton Sand and Gravel Corporation, is located in Hinsdale, Illinois. It is located east of, and directly adjacent to a major highway (I-294) and is bounded to the north and south by 22nd (Cermak Road) and 31st streets, respectively.

The site is a 275-acre landfill that accepted general municipal waste and wastewater treatment sludge from 1959 to 1984. The Illinois Environmental Protection Agency (IEPA) also permitted the disposal of special wastes at the site. The Sexton Corporation is leasing the property from Catholic Cemeteries until 1988. The landfill is no longer in operation.

Some of the special wastes disposed at the landfill include: municipal sludge, oil sludge waste, foundry sand, and slag totaling 56,071 cubic yards. These wastes contain low concentrations (E.P. toxicity) of cyanide, cadmium, nickel, chromium, lead, and zinc.

On October 4, 1984, U.S. EPA personnel sampled eight residential wells to the east of the landfill in which various concentrations of 1,1-dichloroethane were detected. One surface water and three soil/sediment samples were also collected. The surface water sample, collected from a pond to the east of the landfill, contained very low concentrations of heavy metals and chloroform. A background sample was not collected.

Soil samples collected downslope and east of the landfill also contained very low concentrations of heavy metals. However, relatively higher concentrations of organic contaminants were also detected. These contaminants included pentachlorophenol, phenanthrene, fluoranthene, pyrene, benzo(k)fluoranthene, benzo(a)pyrene, indeno(1,2,3-cd)pyrene, benzo(ghi)perylene, and beta-BHC.

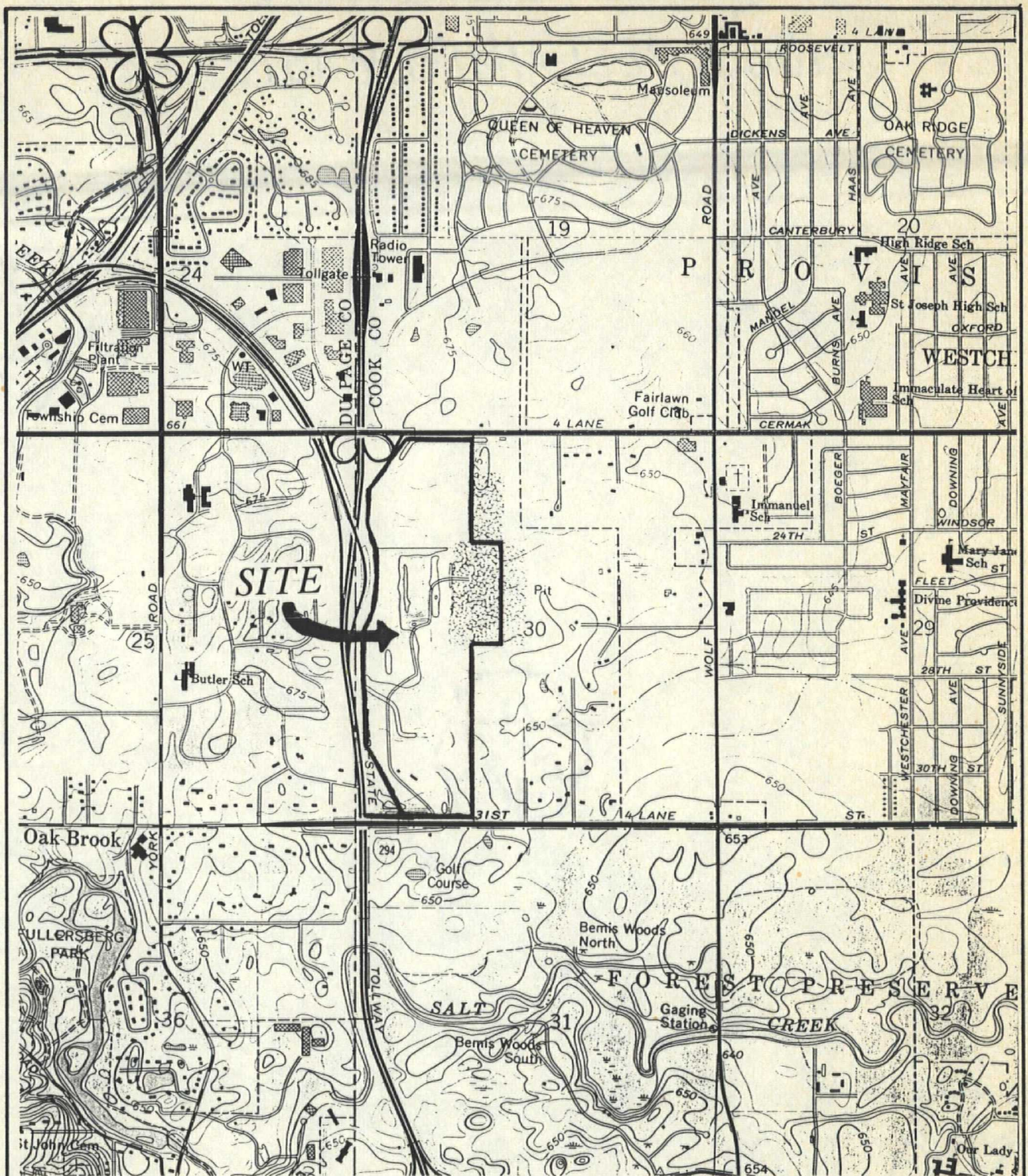
2.2 GEOGRAPHY/PHYSIOGRAPHY

The Hinsdale-Sexton Landfill is located within a large residential area which borders the landfill to the east, west, and north (see Figure 2-1). The site is bordered to the south by the Bemis Woods Forest Preserve. Salt Creek flows west and south of the site. In general, the area topography is characterized by undulating hills of low to little relief with moderate drainage. The landfill itself consists of a relatively high and elongate mound of covered refuse. A pit, observed on a topographic map, is located directly northeast of the landfill. Drainage within the vicinity of the site is directed along unnamed ditches along Cermak Road and I-294 which may eventually reach Salt Creek. An intermittent creek that flows eastward is located east of the site. The landfill slope does not preclude surface runoff.

2.3 GEOLOGY/HYDROGEOLOGY

A review of the current literature indicates the site is underlain by 10 to 100 feet of unconsolidated glacial drift which overlies the Silurian-aged dolomite (Niagaran Formation) (see Appendix A). The site is located over the south bank of a preglacial valley (see Figures 2-2 and 2-3) where the glacial deposits thicken northward toward the valley axis near 24th Street (see Figure 2-2).

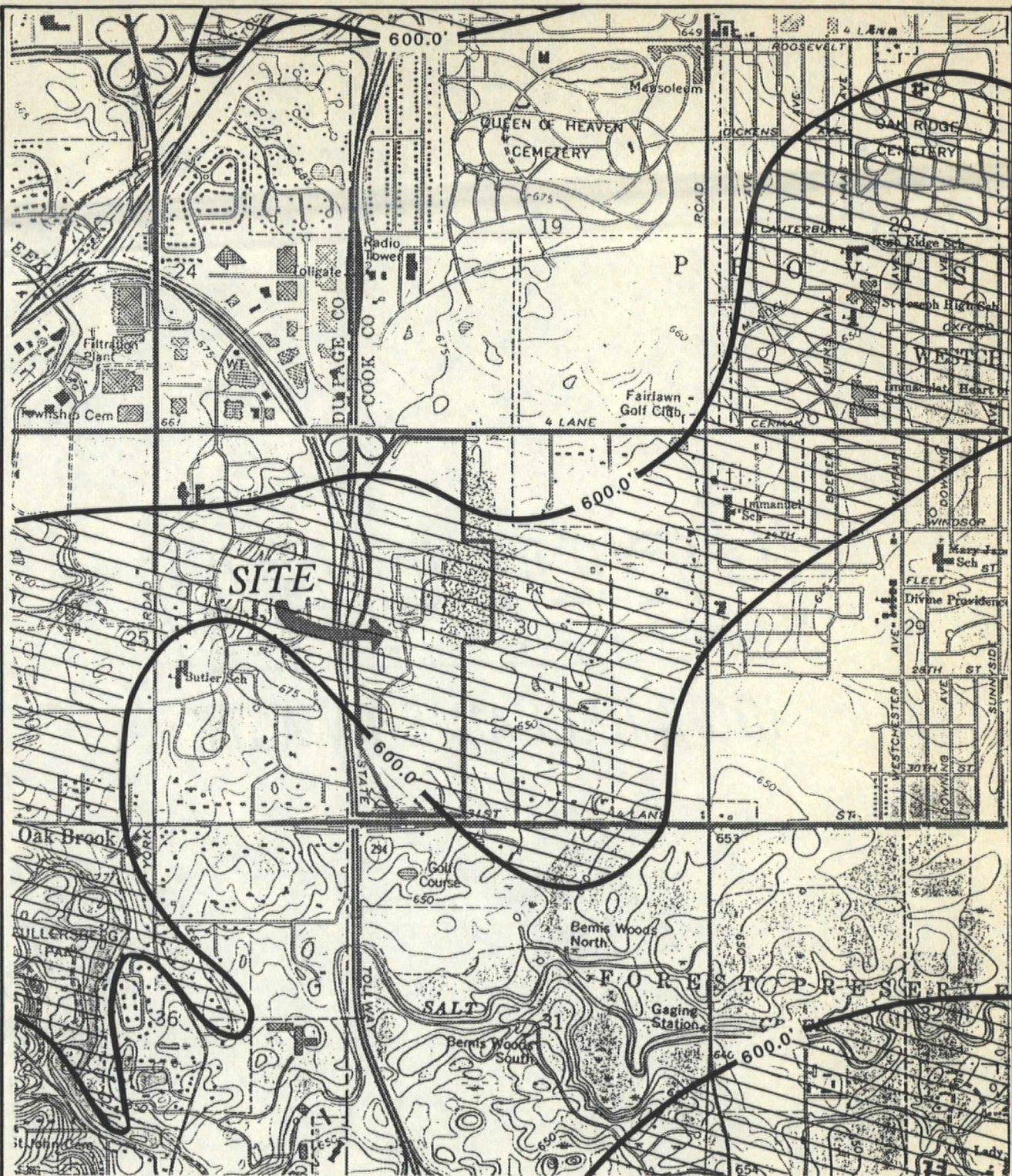
The glacial deposits consist of a differentiated sequence of clay, sand, and silt. The uppermost unit consists of a clay till with isolated thin beds of clayey silt to silt and ranges in thickness from 5 to 37 feet (see Figure 2-4). Underlying the clay till is a sand unit (upper glacial aquifer) that is 10 to 20 feet thick. Below the sand unit is a layer of gray silt to clay with thin beds of sand to silty clay. Deposits underlying these units, and trending along the valley axis, are presently unknown. These deposits may represent an aquifer.



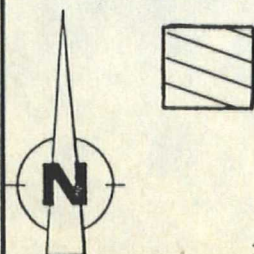
ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE SITE LOCATION MAP		FIGURE # 2-1
SITE HINSDALE SEXTON LANDFILL		SCALE 1:24,000
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE U.S.G.S. QUADRANGLE MAP HINSDALE QUAD.		DATE 1963
		REVISED 1980



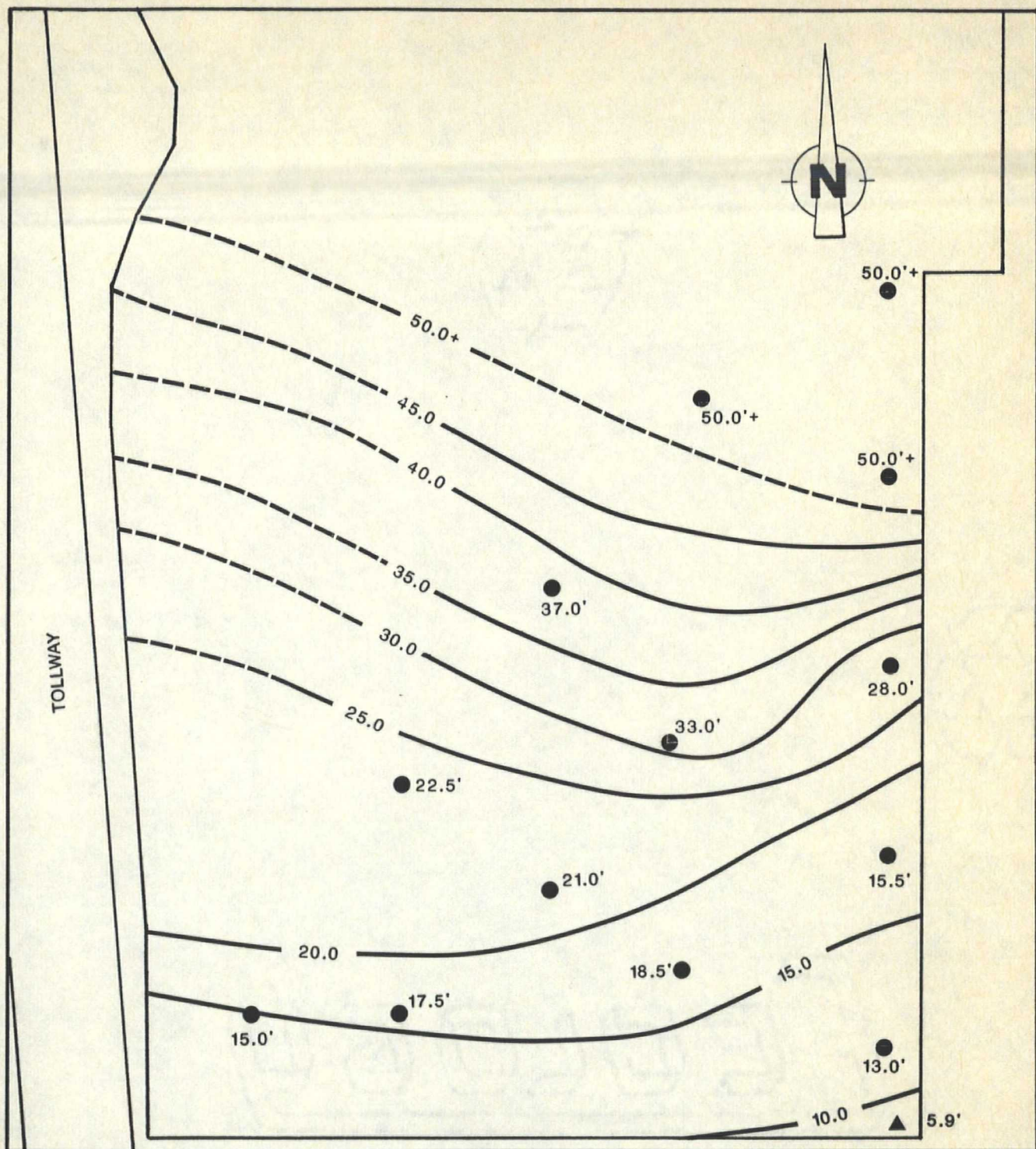
PRE-GLACIAL VALLEY



ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE BEDROCK ELEVATION MAP		FIGURE # 2-2
SITE HINSDALE SEXTON LANDFILL		SCALE 1:24,000
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE PISKIN, 1963; I.S.G.S. AND U.S.G.S. QUADRANGLE MAP HINSDALE QUAD.		DATE 1963 REVISED 1980

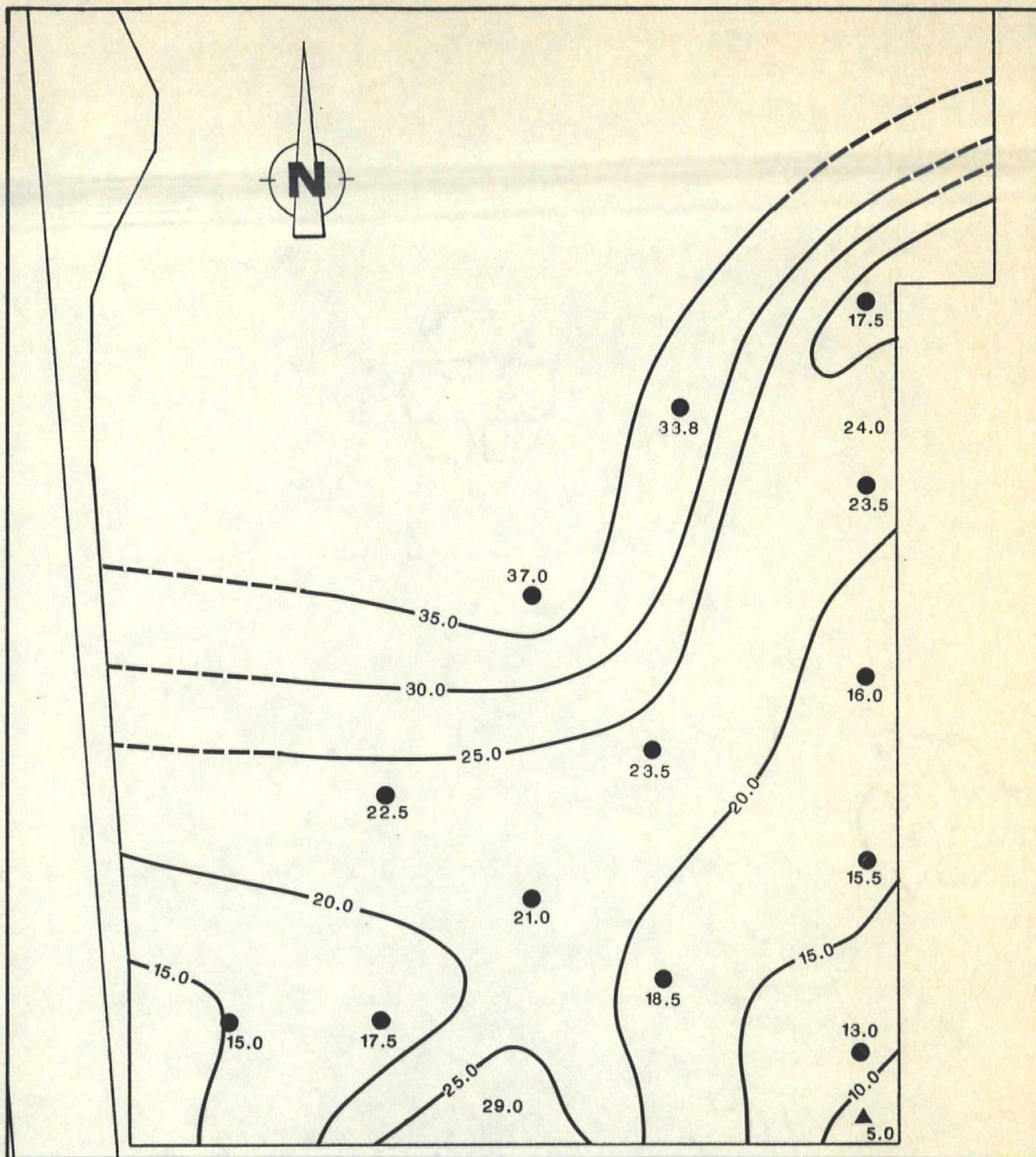


31st STREET

ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE		FIGURE #
STRUCTURE CONTOUR OF THE BEDROCK SURFACE		2-3
SITE		SCALE
HINSDALE SEXTON LANDFILL		1" = 400'
CITY	STATE	P.A.N.
OAKBROOK	ILLINOIS	FIL0041G
SOURCE ECOLOGY AND ENVIRONMENT, INC AND WALTER H. FLOOD AND CO., INC		DATE
		REVISED



ecology and environment, inc.

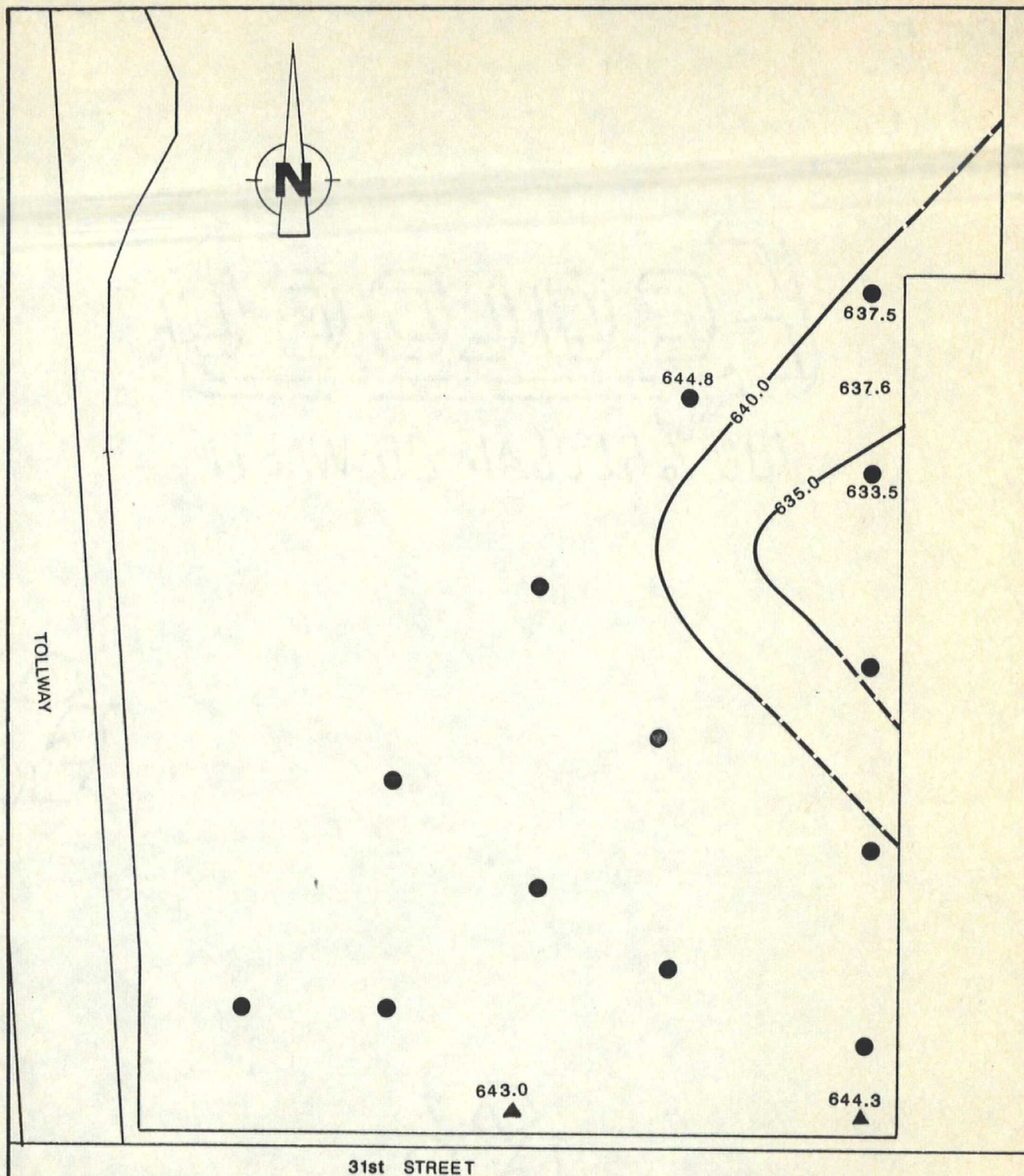
111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE		FIGURE #
ISOPACH OF THE CONFINING UNIT		2-4
SITE		SCALE
HINSDALE SEXTON LANDFILL		1" = 400'
CITY	STATE	P.A.N.
OAKBROOK	ILLINOIS	FIL0041G
SOURCE		DATE
ECOLOGY AND ENVIRONMENT, INC AND WALTER H. FLOOD AND CO., INC		REVISED

The presence of this aquifer could be determined by drilling a well at the valley axis.

Based on data collected from 1972 to 1974, groundwater flow in the glacial aquifers is predicted to be easterly (see Figure 2-5). Based on data collected in 1972, flow in the bedrock aquifer is toward the south-southeast (see Figure 2-6). The location and installation of monitoring wells will be based upon these flow directions. An interconnection between the aquifer(s) of concern has been hypothesized, but no substantial quantitative data are available.

Various residential and municipal wells draw water from the Silurian dolomite aquifer. Usage of both bedrock and glacial aquifers is presently unknown. Currently, only the upper glacial aquifer is monitored at the site.



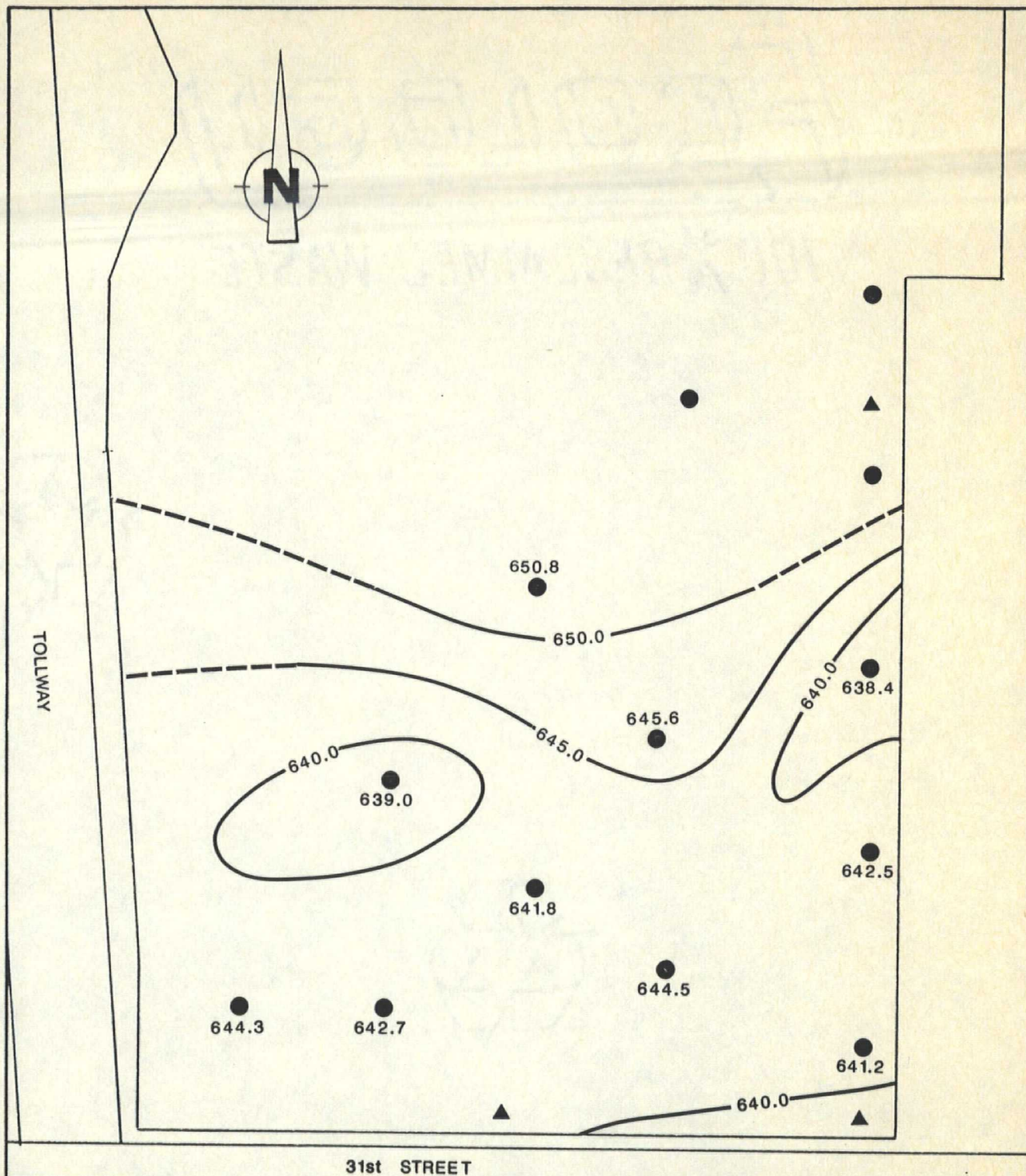
LEGEND

- SOIL BORING
- ▲ WELL
- CONTOUR LINE
(DASHED WHERE
INFERRED)

ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE WATER LEVEL OF THE GLACIAL DRIFT AQUIFER 1972-1974		FIGURE # 2-5
SITE HINSDALE SEXTON LANDFILL		SCALE 1" = 400'
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE ECOLOGY AND ENVIRONMENT, INC AND WALTER H. FLOOD AND CO., INC		DATE
		REVISED



LEGEND

● SOIL BORING

▲ WELL

— CONTOUR LINE
(DASHED WHERE
INFERRED)

ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE WATER DEPTH OF THE SILURIAN DOLOMITE AQUIFER 1972		FIGURE # 2-6
SITE HINSDALE SEXTON LANDFILL		SCALE 1" = 400'
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE ECOLOGY AND ENVIRONMENT, INC AND WALTER H. FLOOD AND CO., INC		DATE
		REVISED

3. PROCEDURES

3.1 INTRODUCTION

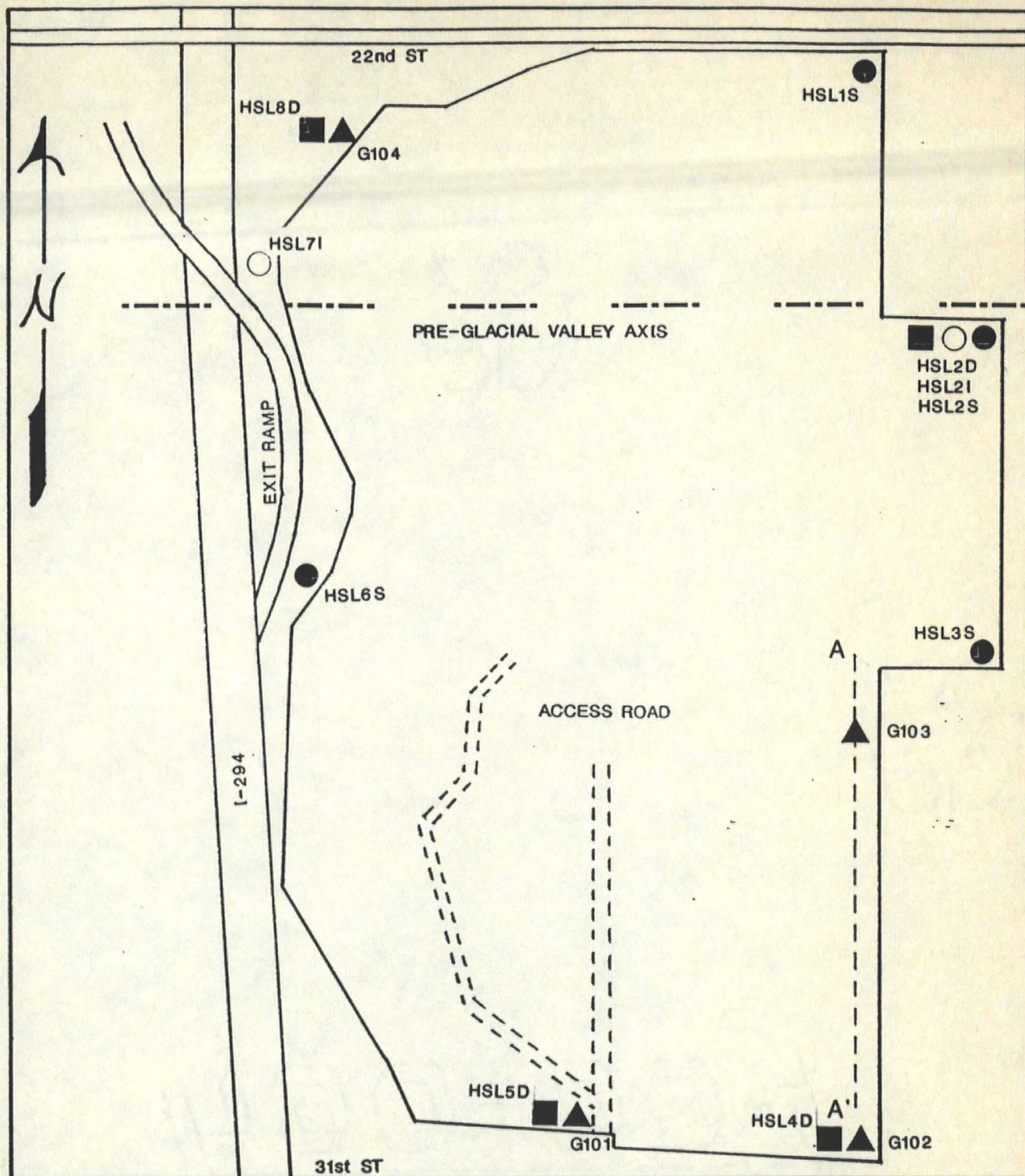
The installation of eight to ten monitoring wells is proposed for the Hinsdale-Sexton Landfill. Ten wells will be installed if an intermediate aquifer is present along the bedrock valley axis. A series of shallow, intermediate, and deep wells will be installed at the respective aquifer depths (see Figures 3-1 and 3-2). Subsurface samples will be sampled at designated intervals. After well completion, all wells will be developed, surveyed, and sampled according to quality assurance/quality control (QA/QC) guidelines. A surface water sampling program will be conducted along surface drainage pathways. Surface soil sampling will also be conducted along these drainage routes. Finally, a pump test is proposed to determine and document the alleged hydraulic connection between aquifers.

3.2 HYDROGEOLOGIC INVESTIGATION

3.2.1 Geophysical Investigation

A preliminary geophysical survey of the eastern portion of the site will be conducted prior to drilling in order to locate the bedrock valley axis. The location and placement of wells HSL2S, HSL2I, HSL2D, and HSL7I will depend upon the results obtained from this survey.

Two overlapping series of transects will be conducted along the east side of the landfill (see Figure 3-3) using a combination of resistivity and seismic survey methods. One continuous series consisting of widely spaced geophones placed along the transect line will be used

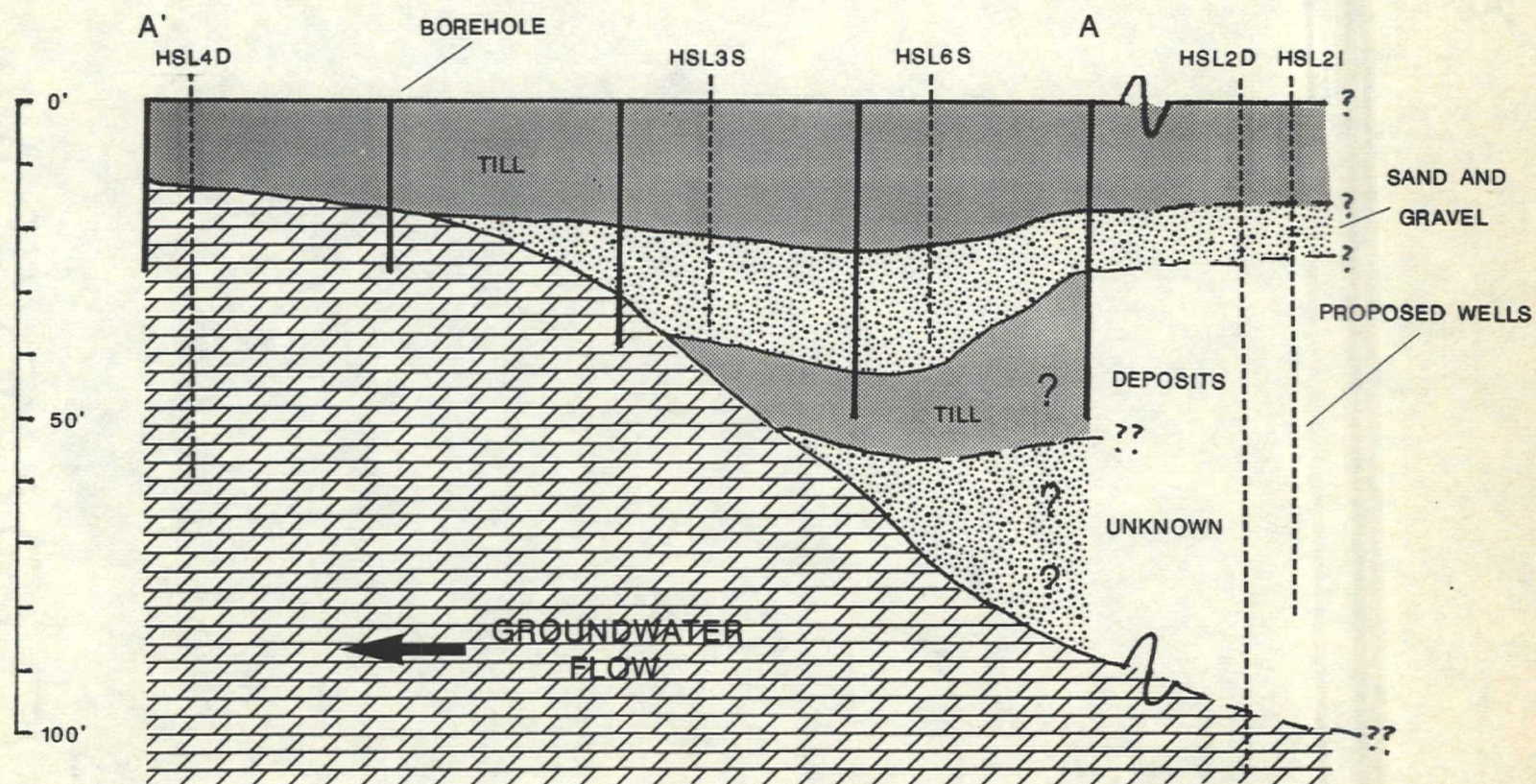


- SHALLOW WELL
- INTERMEDIATE WELL
- DEEP WELL
- ▲ EXISTING SHALLOW WELL

ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

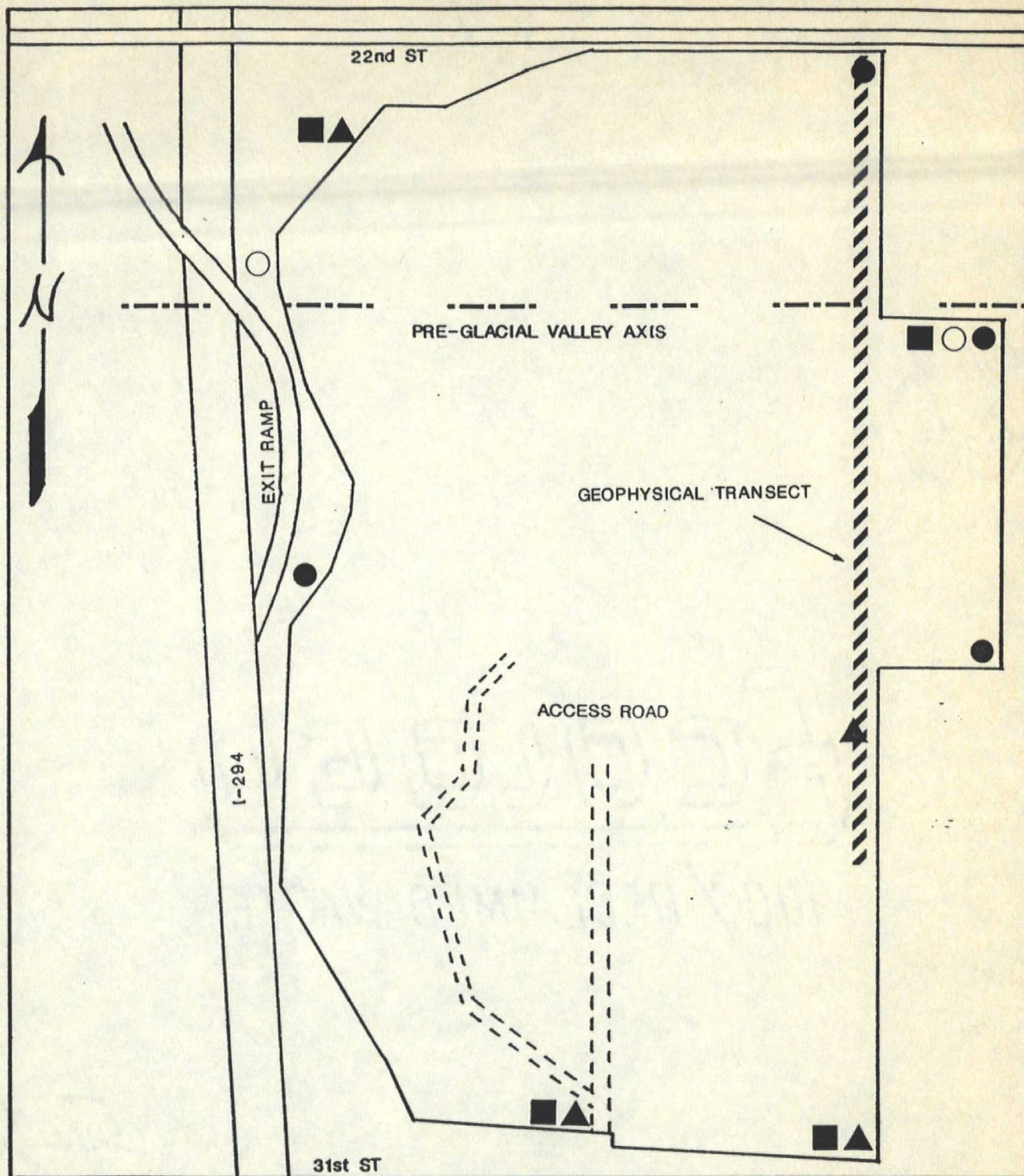
TITLE WELL LOCATION MAP		FIGURE # 3-1
SITE HINSDALE SEXTON LANDFILL		SCALE N.T.S.
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE		DATE
		REVISED



ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE		FIGURE #
GEOLOGIC CROSS-SECTION A to A'		3-2
SITE		SCALE
HINSDALE SEXTON LANDFILL		N.T.S.
CITY	STATE	P.A.N.
OAKBROOK	ILLINOIS	FIL0041G
SOURCE		DATE
		REVISED



- SHALLOW WELL
- INTERMEDIATE WELL
- DEEP WELL
- ▲ EXISTING SHALLOW WELL

ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE GEOPHYSICAL SURVEY LOCATION		FIGURE # 3-3
SITE HINSDALE SEXTON LANDFILL		SCALE N.T.S.
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE		DATE
		REVISED

to define all the stratigraphic boundaries to the bedrock surface. A series of four short discontinuous transects consisting of closely spaced geophones along the same transect line will be used to increase the resolution of the bedrock valley and overlying stratigraphic units. The length of both transects will overlap the proposed locations for wells HSL2S, HSL2I, and HSL2D (see Figure 3-1) to correlate geophysical results with existing stratigraphic data from well G103.

A transect along the west side of the landfill will be considered, but traffic along I-294 may interfere with data retrieval.

3.2.2 Monitoring Well Installation

3.2.2.1 Borehole Placement and Sampling

Eight to ten boreholes/wells will be installed to monitor the glacial and bedrock aquifers. Ten wells will be installed if the pre-glacial valley axis is located and only if a basal valley-fill aquifer is present. Based upon this situation, four shallow, two intermediate, and four deep boreholes/wells will be installed at the site (see Figure 3-1).

Split spoon samples will be collected during borehole advancement at designated intervals in order to log and characterize the subsurface geology. All samples will be continuously screened for contaminants with an organic vapor analyzer (OVA) and shipped to a Contract Laboratory Program (CLP) laboratory for chemical analysis.

Two sampling schemes will be implemented. The first will be used to sample the uppermost till unit in order to characterize the extent, if any, of possible contaminant migration. Continuous sampling will be conducted over a 10-foot interval, followed by sampling at 2.5-foot intervals for another 10 feet, and sampling at 5.0-foot intervals until the shallow aquifer or bedrock is encountered. A minimum of 10 soil samples will be collected for subsurface chemical analysis at each borehole location. The second scheme will be used during borehole advancement to collect samples to characterize the subsurface stratigraphy. Samples will be collected at 5.0-foot intervals below the upper till unit. Samples not collected for chemical analysis will be further analyzed for logging purposes. Eight Shelby tube samples will be collected from the shallow till unit encountered during drilling. Three

more samples will be collected from the deeper till unit. All Shelby tube samples will be analyzed for grain size and permeability.

3.2.2.2 Monitoring Well Construction

The shallow wells will be placed in the upper sand aquifer (see Figure 3-2) with one upgradient (HSL6s) and three downgradient (HSL1S, -2S, -3S) wells. The shallow wells will be drilled, precluding the presence of cobbles and boulders, with an 8-inch continuous flight, hollow-stem auger. Well materials will consist of 2-inch inside diameter (ID) stainless steel riser pipe with threaded flush joints and 10-foot-long screens of manufactured continuous wire-wound design with a screen size of 0.01 inches. The well screens will be placed at a depth of 5 feet below the upper till unit. The depth of each shallow well will vary according to the depth of the upper sand unit (see Figure 3-2). The locations of the shallow wells are subject to change, depending upon the present groundwater flow direction.

The intermediate wells will be placed at a depth within the lower sand aquifer (if present) along the bedrock valley axis (see Figure 3-2). There will be one upgradient well (HSL7I) and one downgradient well (HSL2I) (see Figure 3-1). Well construction materials are similar to those listed above, however, additional materials will be needed to prevent cross-contamination of the upper and lower (if present) glacial aquifers prior to final well installation. The 10-inch boreholes will be cased with 6 5/8-inch outside diameter (OD) steel casing with threaded joints to the base of the upper sand unit. The casing will be driven a minimum of 1 foot into the underlying till member. At this point, the outer casing annulus will be grouted and allowed to set for at least 24 hours. Boreholes will be advanced with a 5-inch bit until a lower glacial aquifer is encountered. The intermediate wells will be drilled using the rotary mud method.

The deep (bedrock) wells (see Figure 3-1) will be placed at a depth of no less than 50 and no greater than 130 feet (see Figure 3-2). One upgradient (HSL8D) and two downgradient (HSL4D and HSL5D) wells will be installed. A fourth deep well (HSL2D) will be located along the valley axis. Wells HSL4D and HSL5D will be placed at a depth no more than 30 feet below the base of the upper sand unit. Wells HSL2D and HSL8D will

be placed at a depth no greater than 20 feet below the bedrock surface. All deep wells will be drilled using a combination of rotary-mud (overburden) and combination coring/rotary-mud (bedrock) because of the thick glacial overburden. Well construction materials for final well installation will be similar to those discussed above.

In order to prevent the potential of cross-contamination between aquifers during drilling of the wells HSL2D and HSL8D, the boreholes drilled to the bedrock aquifer will be double-cased. The 10-inch borehole will be cased with 8 5/8-inch OD steel casing with threaded joints to the base of the upper sand unit. The casing will be driven a minimum of 1 foot into the lower till unit where the outer annulus will be grouted and allowed to set. The borehole will be advanced with an 8 1/2-inch bit to a minimum of 1 foot into the bedrock surface. Next, the 8 1/2-inch borehole will be cased with 6 5/8-inch OD steel casing with threaded joints into the bedrock surface. The middle annulus will be grouted and allowed to set accordingly. The remainder of the 6-inch borehole will be cored with a NQ core barrel and reamed with a 6-inch bit to well completion.

Prior to coring HSL4D and HSL5D, the clay overburden will be drilled to bedrock with a hollow-stem auger until nonfractured bedrock is reached. Permanent steel casing (6 5/8-inch OD) will be anchored into bedrock and the outer annulus grouted accordingly. HSL4D and HSL5D will then be cored from the top of the bedrock to final depth, using an NQ wire-line barrel. The boreholes will then be reamed with a 6-inch bit until well completion. Depending upon the fracture density of the bedrock and resulting grout loss, the borehole may have to be cased prior to riser pipe installation. All core samples will be marked indicating location and depths, and packaged and studied in detail at a later time.

The remaining annular space for each well will be filled using the following materials, starting from the bottom:

- 1) Clean 3/8-inch diameter gravel covering the screen and extending 3 feet above the top of the screen.

- 2) Clean fine-grained sand placed to a minimum of 1 foot above the gravel pack.
- 3) Volclay grout placed through tremie pipe from the top of the fine sand seal to the ground surface.

The 2-inch OD stainless steel riser pipe will have a 2.5-foot stick-up ending in threads and will be covered with a 5-foot-long, 5-inch ID, protective steel casing with locking cap. A concrete plug and pad which slopes away from the steel casing will also be installed. Concrete-filled steel bumper guards, 4-inch ID, will be installed as needed.

3.3 AQUIFER TESTING

3.3.1 Physical Testing

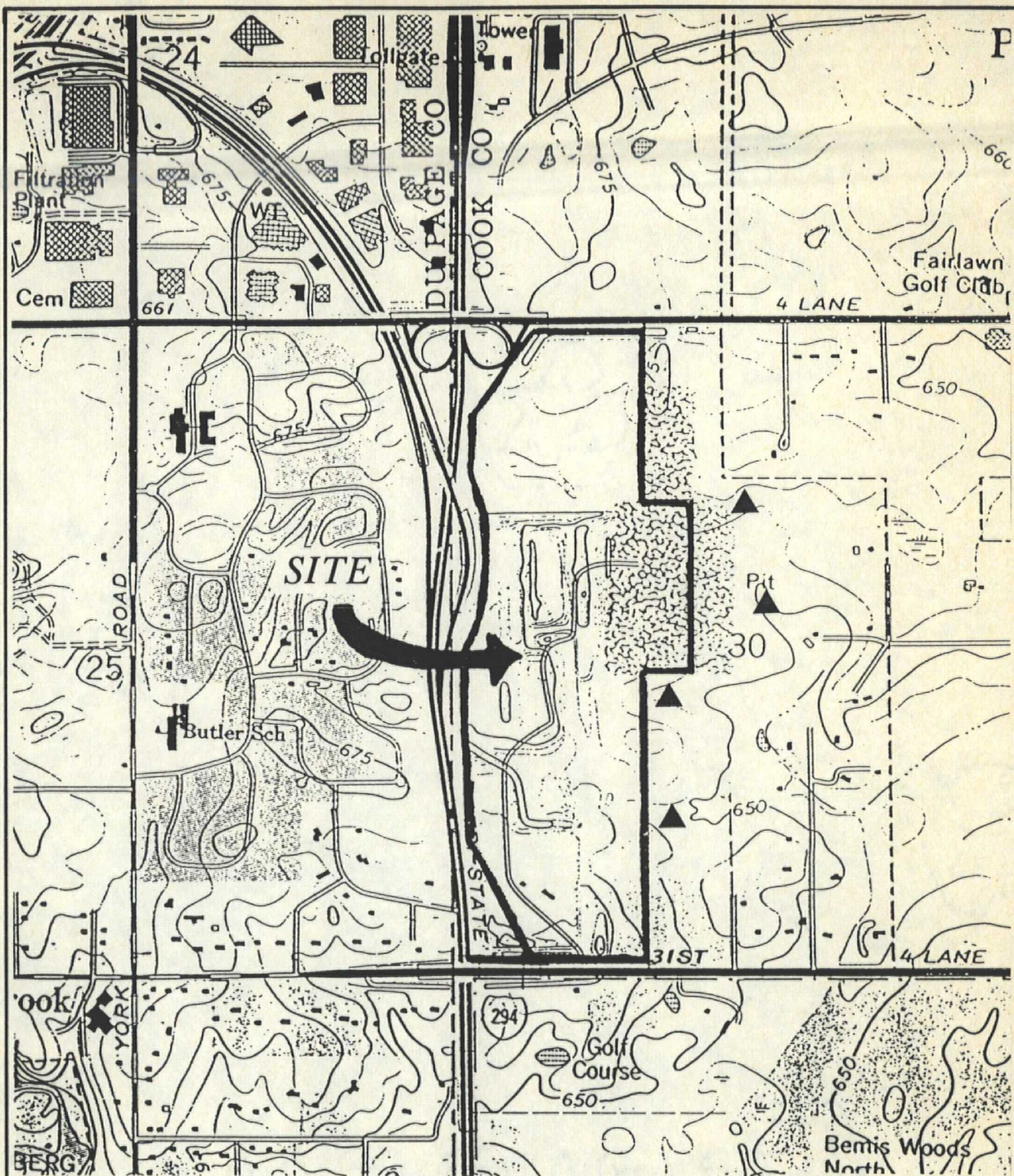
Water elevations will be recorded for each monitoring well and used to calculate groundwater flow direction and gradient. Rising head slug tests will also be performed to assess additional physical characteristics of the aquifer.

3.3.2 Chemical Testing

Upon completion and development of all of the proposed wells, groundwater samples from each well will be collected and sent to designated CLP laboratories for analysis. The samples will be analyzed for organic and inorganic target compounds.

3.4 SURFACE SOIL/SEDIMENT SAMPLING

Four to six surficial soil and sediment samples will be collected on and around the site, primarily along surface runoff paths (see Figure 3-4). The locations and number of samples will be subject to change depending upon site observations during the project. These samples will be shipped to CLP laboratories for chemical analysis. The samples will be analyzed for organic and inorganic target compounds and will be used to characterize contaminants that may be originating from the site.



ecology and environment, inc.

111 WEST JACKSON BLVD., CHICAGO, ILLINOIS 60604, TEL. 312-663-9415

TITLE PROPOSED SOIL SAMPLE LOCATION MAP		FIGURE # 3-4
SITE HINSDALE SEXTON LANDFILL		SCALE 1:1200
CITY OAKBROOK	STATE ILLINOIS	P.A.N. FIL0041G
SOURCE U.S.G.S. QUADRANGLE MAP HINSDALE QUAD.		DATE 1963
		REVISED 1980

3.5 SURFACE WATER SAMPLING

Four to six upstream and downstream water samples will be collected along the unnamed ditches bordering the site and at the intermittent tributary, if applicable, of Salt Creek. The locations and number of samples will also be subject to change as mentioned above. These samples will be shipped to the CLP laboratories for chemical analysis. The samples will be analyzed for organic and inorganic target compounds.

APPENDIX A

BORING LOGS

FOR: Sexton Filling & Grading Corporation		SOIL BORING LOG NO. 1	
PROJECT: 12100 West. 31st Street		WALTER H. FLOOD & CO., INC.	
LOCATION Westchester, Illinois		• Engineers •	
METHOD OF BORING: A & C		• CHICAGO • KALAMAZOO •	
SPLIT SPOON SIZE: 2 IN.		DATE OF BORING: 3-7-72	
WT. OF HAMMER 140 LBS.		BY: BJ,JC,MC:bc	
INCH DROP 30		JOB NO.: 7205-0010	
SHELBY TUBE SIZE		VERTICAL SCALE: 1"=10'	
CASING USED 15'-24" IDHS			
WATER LEVEL READINGS			
Dry W.D.			
B.C.R.			
8.0' A.C.R.			
9.2'@24 HRS. AFTER DRILLING			
HRS. AFTER DRILLING			

ELEV.	DEPTH	S	T	N	LF	DD	DESCRIPTION	Qu • LABORATORY X 1000	O PENETROMETER			
								2	4	6	8	10
650.4	0.0						Ground surface					
		1	ss	8			Brown&black clay, fill	3000				
646.9	3.5	2	ss	12			Black clay, very tough			31.6		
640.9	6.0	3	ss	16			Brown to gray clay, trace of small gravel, very tough to hard	19.0	23.8	7500	9000+	
		4	ss	40								
		5	ss	50/4								
637.4	13.0	6	ss	100/1"			Brownish-gray dolomite, weathered, fractured, dense	13.4			9000+	
		7	ss	100/1"				11.8				
		8	C									
		9	C									
624.4	26.0						End of boring					

ELEV.	DEPTH	S	T	N	LF	DD	DESCRIPTION	10	20	30	40	50
								Wc	▲ NATURAL			

LEGEND:

DEPTH—FEET BELOW GROUND SURFACE

S — SAMPLE NUMBER

T — TYPE OF SAMPLE

N — PENETRATION, BLOWS PER FOOT

L — SAMPLE LENGTH

R — LENGTH OF SAMPLE RECOVERED

DD — DRY DENSITY, LB. PER CU. FOOT

WO — WASHOUT

A — AUGER

HS — HOLLOW STEM AUGER

SS — SPLIT SPOON

ST — SHELBY TUBE

FT — FISH TAIL

C — CORE

BCR— BEFORE CASING REMOVAL

ACR— AFTER CASING REMOVAL

WD — WHILE DRILLING

WCI — WET CAVE IN

DCI — DRY CAVE IN

Qu — UNCONFINED COMPRESSIVE STRENGTH POUNDS PER SQUARE FOOT

BEDROCK

FOR: Sexton Filling & Grading Corporation							SOIL BORING LOG NO. 2				
PROJECT: 12100 West 31st Street							WALTER H. FLOOD & CO., INC.				
LOCATION: Westchester, Illinois							• Engineers •				
METHOD OF BORING: A & C							• CHICAGO • KALAMAZOO •				
SPLIT SPOON SIZE: 2 IN.							WATER LEVEL READINGS				
WT. OF HAMMER 140 LBS.							Dry W.D.				
INCH DROP 30							B.C.R.				
SHELBY TUBE SIZE							12.6' A.C.R.				
CASING USED 15'-2 1/4" IDHS							10.5' @ 24 HRS. AFTER DRILLING				
							HRS. AFTER DRILLING				
DATE OF BORING: 3-9-72							BY: BJ, CN, JC:bc				
JOB NO.: 7205-0010							VERTICAL SCALE: 1"=10'				

ELEV.	DEPTH	S	T	N	L	R	DD	DESCRIPTION	Qu • LABORATORY O PENETROMETER X 1000					
									2	4	6	8	10	
653.0	0.0							Ground surface						
652.0	1.0	1	ss	26				Black clay loam						
		2	ss	28				Brown and gray clay, trace of small gravel, hard	20.2					08500
		3	ss	34					19.3					9000+
		4	ss	20					18.2					9000+
642.0	11.0	5	ss	27				Gray clayey silt, medium dense	17.1					
639.5	13.5	6	ss	150				See note	11.1					
637.5	15.5	7	C					Brown to gray dolomite, thinly bedded, fractured, dense	11.1					
626.5	26.5							End of boring						
								Note: Gray clayey silt, some small to large gravel, stone fragments, dense						

ELEV.	DEPTH	S	T	N	L	R	DD	DESCRIPTION	10	20	30	40	50
									Wc	▲ NATURAL			

LEGEND: DEPTH—FEET BELOW GROUND SURFACE				WO — WASHOUT				BCR — BEFORE CASING REMOVAL			
S — SAMPLE NUMBER				A — AUGER				ACR — AFTER CASING REMOVAL			
T — TYPE OF SAMPLE				HS — HOLLOW STEM AUGER				WD — WHILE DRILLING			
N — PENETRATION, BLOWS PER FOOT				SS — SPLIT SPOON				WCI — WET CAVE IN			
L — SAMPLE LENGTH				ST — SHELBY TUBE				DCI — DRY CAVE IN			
R — LENGTH OF SAMPLE RECOVERED				FT — FISH TAIL				Qu — UNCONFINED COMPRESSIVE STRENGTH			
DD — DRY DENSITY, LB. PER CU. FOOT				C — CORE				POUNDS PER SQUARE FOOT			

FOR: Sexton Filling & Grading Corporation

PROJECT: 12100 West 31st Street

LOCATION Westchester, Illinois

METHOD OF BORING: A
SPLIT SPOON SIZE: 2 IN.
WT. OF HAMMER 140 LBS.
INCH DROP 30
SHELBY TUBE SIZE
CASING USED 30'-2 1/4" IDHS

WATER LEVEL READINGS
17.0' W.D.
B.C.R.
11.0' A.C.R.
10.0' @ 24 HRS. AFTER DRILLING
HRS. AFTER DRILLING

SOIL BORING LOG NO. 3

WALTER H. FLOOD & CO., INC.

• Engineers •

• CHICAGO • KALAMAZOO •

DATE OF BORING: 3-9-72

BY: CN&JC:bc

JOB NO.: 7205-0010

VERTICAL SCALE: 1"=10'

ELEV.	DEPTH	S	T	N	LR	DD	DESCRIPTION	Qu • LABORATORY X 1000	O PENETROMETER
648.4	0.0						Ground surface		
647.4	1.0	1	ss	16			Black clay loam		
		2	ss	8			Brown and gray clay, very tough	4500	22.0
		3	ss	9				5000	23.2
639.9	8.5	4	ss	23			Brown and gray clay, trace of small gravel, hard to very tough	22.0	25.3
		5	ss	18				14.4	4000
632.4	16.0	6	ss	20				15.2	4000
629.9	18.5	7	ss	24			Gray fine to medium sand, some silt, medium dense		23.8
		8	ss	27			Gray fine sand and silt, medium dense		
		9	ss	19				13.1	
		10	ss	16					
622.4	26.0	11	ss	22			See note		
620.4	28.0	12	ss	100/1-5			Light gray and brown dolomite thinly bedded, very dense		
		13	C						
		14	C						
610.4	38.0						End of boring		
							Note; Gray silt, some small to large gravel, stone fragments, very dense		
ELEV.	DEPTH	S	T	N	LR	DD	DESCRIPTION	10	20
								30	40
								50	

LEGEND: DEPTH—FEET BELOW GROUND SURFACE
S — SAMPLE NUMBER
T — TYPE OF SAMPLE
N — PENETRATION, BLOWS PER FOOT
L — SAMPLE LENGTH
R — LENGTH OF SAMPLE RECOVERED
DD — DRY DENSITY, LB. PER CU. FOOT

WO — WASHOUT
A — AUGER
HS — HOLLOW STEM AUGER
SS — SPLIT SPOON
ST — SHELBY TUBE
FT — FISH TAIL
C — CORE
Wc — WATER CONTENT PERCENT

BCR — BEFORE CASING REMOVAL
ACR — AFTER CASING REMOVAL
WD — WHILE DRILLING
WCI — WET CAVE IN
DCI — DRY CAVE IN
Qu — UNCONFINED COMPRESSIVE STRENGTH
POUNDS PER SQUARE FOOT

FOR: Sexton Filling & Grading Corporation						SOIL BORING LOG NO. 4					
PROJECT: 12100 West 31st Street						WALTER H. FLOOD & CO., INC.					
LOCATION Westchester, Illinois						• Engineers •					
METHOD OF BORING: HS			WATER LEVEL READINGS			DATE OF BORING: 3-16-72			BY: BJ&JA:bc		
SPLIT SPOON SIZE: 2 IN.			18.5' W.D.			JOB NO.: 7205-0010			VERTICAL SCALE: 1"=10'		
WT. OF HAMMER 140 LBS.			18.0' B.C.R.								
INCH DROP 30			17.0' A.C.R.								
SHELBY TUBE SIZE			16.7' @ 24 HRS. AFTER DRILLING								
CASING USED 50'-2 1/4" IDHS			HRS. AFTER DRILLING								

ELEV.	DEPTH	S	T	N	L	R	DO	DESCRIPTION	Qu • LABORATORY O PENETROMETER X 1000					
									2	4	6	8	10	
650.2	0.0							Ground surface						
648.7	1.5	1	ss	10				Black clay loam						
		2	ss	13				Brown and gray clay, very tough	4000	20.2	25.6		8000	
		3	ss	15					19.3					
641.7	8.5	4	ss	28				Brown to gray clay, trace of small gravel, hard to very tough	17.9		5500		9000+	
		5	ss	19					19.0		5500			
		6	ss	12					3200		23.2			
		7	ss	14					20.8					
		8	ss	14					14.9		4500			
		9	ss	11							4000			
626.7	23.5	10	ss	21				Gray medium sand, trace of silt, medium dense	16.3					
		11	ss	32										
621.7	28.5	12	ss	48				Gray fine sand, some silt, dense						
		13	ss	25										
		14	ss	31										
		15	ss	26										
		16	ss	18										
		17	ss	20										
606.7	43.5	18	ss	53				Gray silt, some fine to coarse sand with small to large gravel, occasional boulder, very dense	16.6					
		19	ss	53										
600.2	50.0	20	ss	67				End of boring						

ELEV.	DEPTH	S	T	N	L	R	DO	DESCRIPTION	10	20	30	40	50
									Wc ▲ NATURAL				

LEGEND:

DEPTH - FEET BELOW GROUND SURFACE

S - SAMPLE NUMBER

T - TYPE OF SAMPLE

N - PENETRATION, BLOWS PER FOOT

L - SAMPLE LENGTH

R - LENGTH OF SAMPLE RECOVERED

DO - DRY DENSITY, LB. PER CU. FOOT

WO - WASHOUT

A - AUGER

HS - HOLLOW STEM AUGER

SS - SPLIT SPOON

ST - SHELBY TUBE

FT - FISH TAIL

C - CORE

Wc - WATER CONTENT PERCENT

BCR - BEFORE CASING REMOVAL

ACR - AFTER CASING REMOVAL

WD - WHILE DRILLING

WCI - WET CAVE IN

DCI - DRY CAVE IN

Qu - UNCONFINED COMPRESSIVE STRENGTH POUNDS PER SQUARE FOOT

FOR: Sexton Filling & Grading Corporation						SOIL BORING LOG NO. 5					
PROJECT: 12100 West 31st Street						WALTER H. FLOOD & CO., INC.					
LOCATION: Westchester, Illinois						• Engineers •					
METHOD OF BORING: HS			WATER LEVEL READINGS			• CHICAGO • KALAMAZOO •					
SPLIT SPOON SIZE: 2 IN.			15.0' W.D.			DATE OF BORING: 5-8-72			BY: DL&BS:bc		
WT. OF HAMMER 140 LBS.			15.0' B.C.R.			JOB NO.: 7205-0010			VERTICAL SCALE: 1"=10'		
INCH DROP 30			14.2' A.C.R.								
SHELBY TUBE SIZE			12.1' @ 24 HRS. AFTER DRILLING								
CASING USED			HRS. AFTER DRILLING								

ELEV.	DEPTH	S	T	N	L	R	DD	DESCRIPTION	Qu • LABORATORY X 1000 Q PENETROMETER					
									2	4	6	8	10	
649.6	0.0							Ground surface						
		1	ss	15				Brown and gray clay, trace of small gravel, very tough	19.2			6000		
		2	ss	13					21.7			6000		
		3	ss	8					4000		23.2			
		4	ss	9					18.8		4000			
639.6	10.0	5	ss	20				Gray silt, clay and medium sand layers, medium dense	2000		22.0			
		6	ss	13										
634.6	15.0	7	ss	18				Gray clay, trace of small gravel, hard		15.1			9000+	
632.1	17.5	8	ss	21				Gray medium to coarse sand, some silt, clay, medium dense						
629.6	20.0	9	ss	31				Gray fine sand and silt, dense						
		10	ss	83										
		11	ss	77										
622.1	27.5	12	ss	13				Gray clay, thin sand layers, very tough		21.0				
619.6	30.0	13	ss	48				Gray medium sand, trace of silt, dense				4500		
617.1	32.5	14	ss	9				Gray silty clay, trace of small gravel, tough to very tough	2000	15.1			8000	
		15	ss	29						13.7				
612.1	37.5	16	ss	34				Gray silt, some fine to coarse sand, small to large gravel, occasional boulder, very dense						
		17	ss	101										
		18	ss	61										
		19	ss	125										
		20	ss	104										
		21	ss	145										
599.6	50.0							End of boring						

ELEV.	DEPTH	S	T	N	L	R	DD	DESCRIPTION	10	20	30	40	50
									Wc ▲ NATURAL				

LEGEND: DEPTH—FEET BELOW GROUND SURFACE

S — SAMPLE NUMBER

T — TYPE OF SAMPLE

N — PENETRATION, BLOWS PER FOOT

L — SAMPLE LENGTH

R — LENGTH OF SAMPLE RECOVERED

DD — DRY DENSITY, LB. PER CU. FOOT

WO — WASHOUT

A — AUGER

HS — HOLLOW STEM AUGER

SS — SPLIT SPOON

ST — SHELBY TUBE

FT — FISH TAIL

C — CORE

Wc — WATER CONTENT PERCENT

BCR — BEFORE CASING REMOVAL

ACR — AFTER CASING REMOVAL

WD — WHILE DRILLING

WCI — WET CAVE IN

DCI — DRY CAVE IN

Qu — UNCONFINED COMPRESSIVE STRENGTH POUNDS PER SQUARE FOOT

BEDOCK

FOR: Sexton Filling & Grading Corporation							SOIL BORING LOG NO. 6				
PROJECT: 12100 West 31st Street							WALTER H. FLOOD & CO., INC.				
LOCATION: Westchester, Illinois							• Engineers •				
METHOD OF BORING: HS				WATER LEVEL READINGS			• CHICAGO • KALAMAZOO •				
SPLIT SPOON SIZE: 2 IN.				Dry W.D.			DATE OF BORING: 3-9-72				
WT. OF HAMMER 140 LBS.				B.C.R.			BY: BJ&JA:bc				
INCH DROP 30				Dry A.C.R.			JOB NO.: 7205-0010				
SHELBY TUBE SIZE				14.5' @ 24 HRS. AFTER DRILLING			VERTICAL SCALE: 1"=10'				
CASING USED 18'-2 1/2" IDHS				HRS. AFTER DRILLING							

ELEV.	DEPTH	S	T	N	LR	DO	DESCRIPTION	Qu • LABORATORY X 1000	O PENETROMETER			
								2	4	6	8	10
659.0	0.0						Ground surface					
		1	ss	16			Brown and gray clay, trace of small gravel, hard		19.9			9000+
		2	ss	21				8.0	19.3			9000+
652.0	7.0	3	ss	42			See note 1		17.4			9000+
650.5	8.5	4	ss	17			Brown to gray clay, trace of small gravel, hard					9000+
		5	ss	22					14.2			9000+
		6	ss	33					11.8			8500
643.0	16.0	7	ss	50/5			See note 2	9.2				
640.5	18.5	8	C				Light gray and brown dolomite thinly bedded, fractured, very dense					
		9	C									
		10	C									
625.5	33.5						End of boring					
							Notel: Brown silt, trace of clay, dense					
							Note2: Gray silt, some fine to coarse sand, small to large gravel, stone fragments very dense					

ELEV.	DEPTH	S	T	N	LR	DO	DESCRIPTION	10	20	30	40	50
								Wc	▲ NATURAL			

LEGEND: DEPTH—FEET BELOW GROUND SURFACE				WO — WASHOUT				BCR — BEFORE CASING REMOVAL			
S — SAMPLE NUMBER				A — AUGER				ACR — AFTER CASING REMOVAL			
T — TYPE OF SAMPLE				HS — HOLLOW STEM AUGER				WD — WHILE DRILLING			
N — PENETRATION, BLOWS PER FOOT				SS — SPLIT SPOON				WCI — WET CAVE IN			
L — SAMPLE LENGTH				ST — SHELBY TUBE				DCI — DRY CAVE IN			
R — LENGTH OF SAMPLE RECOVERED				FT — FISH TAIL				Qu — UNCONFINED COMPRESSIVE STRENGTH			
DO — DRY DENSITY, LB. PER CU. FOOT				C — CORE				POUNDS PER SQUARE FOOT			
				Wc — WATER CONTENT PERCENT							

FOR: Sexton Filling & Grading Corporation

SOIL BORING LOG NO. 7

PROJECT: 12100 West 31st Street

WALTER H. FLOOD & CO., INC.

LOCATION Westchester, Illinois

• **Engineers** •

• CHICAGO • KALAMAZOO •

METHOD OF BORING: HS

WATER LEVEL READINGS

SPLIT SPOON SIZE: 2 IN.

23.5' W.D.

WT. OF HAMMER 140 LBS.

17.7' B.C.R.

INCH DROP 30

10.0' A.C.R.

SHELBY TUBE SIZE

11.4' @ 24 HRS. AFTER DRILLING

CASING USED 33'-2 1/4" IDHS

HRS. AFTER DRILLING

DATE OF BORING: 3-15-72

BY: BJ&JA:bc

JOB NO.: 7205-0010

**VERTICAL
SCALE: 1"=10'**

[illegible]

LEGEND: DEPTH—FEET BELOW GROUND SURFACE
S —SAMPLE NUMBER
T —TYPE OF SAMPLE
N —PENETRATION, BLOWS PER FOOT
L —SAMPLE LENGTH
R —LENGTH OF SAMPLE RECOVERED
DD —DRY DENSITY, LB. PER CU. FOOT

WO	- WASHOUT	BCF
A	- AUGER	ACI
HS	- HOLLOW STEM AUGER	WD
SS	- SPLIT SPOON	WCI
ST	- SHELBY TUBE	DCI
FT	- FISH TAIL	Qu
C	- CORE	
Wc	- WATER CONTENT PERCENT	

BCR—BEFORE CASING REMOVAL
ACR—AFTER CASING REMOVAL
WD —WHILE DRILLING
WCI —WET CAVE IN
DCI — DRY CAVE IN
Qu — UNCONFINED COMPRESSIVE STRENGTH
POUNDS PER SQUARE FOOT

FOR: Sexton Filling & Grading Corporation							SOIL BORING LOG NO. 8				
PROJECT: 12100 West 31st Street							WALTER H. FLOOD & CO., INC.				
LOCATION Westchester, Illinois							• Engineers •				
METHOD OF BORING: HS				WATER LEVEL READINGS			DATE OF BORING: 3-16-72			BY: BJ&JA:bc	
SPLIT SPOON SIZE: 2 IN.				31.0' W.D.			JOB NO.: 7205-0010			VERTICAL SCALE: 1"=10'	
WT. OF HAMMER 140 LBS.				46.6' B.C.R.							
INCH DROP 30				29.0' A.C.R.							
SHELBY TUBE SIZE				16.2' @ 24 HRS. AFTER DRILLING							
CASING USED 50'-2 1/4" IDHS				HRS. AFTER DRILLING							

ELEV.	DEPTH	S	T	N	L	R	DO	DESCRIPTION	Qu • LABORATORY X 1000	O PENETROMETER			
									2	4	6	8	10
661.0	0.0							Ground surface					
		1	ss	19				Brown and gray clay, trace of small gravel, hard to very tough		26.3			
		2	ss	27					17.6	5500		9000+	
		3	ss	28						18.2		9000+	
		4	ss	31						17.9		9000+	
		5	ss	25						19.6		9000+	
		6	ss	14						20.8	4200		
645.0	16.0	7	ss	10				Gray clay, trace of small to large gravel, occasional sand layer, tough to hard	2500	15.2			
		8	ss	16					15.2		6000		
		9	ss	17					15.5	3500			
627.2	33.8	10	ss	29				Coarse sand layer		12.6			
626.5	34.5							See note					
624.5	36.5	11	ss	106				Gray fine sand and silt, dense	9.9	15.7	5000		
		12	ss	14							4500		
620.0	41.0	13	ss	69				Gray clay, trace of small to large gravel, very tough		12.6	3000		
617.5	43.5	14	ss	54				Gray silt, some fine to medium sand, small to large gravel, boulders, very dense	9.9		5000		
		15	ss	39						3700		29.9	
		16	ss	50									
		17	ss	39					9.4	12.0	5000		
		18	ss	77						14.4			
		19	ss	126						13.4			
611.0	50.0	20	ss	100				End of boring	9.4				
								Note: Gray clay, trace of small gravel, tough to very tough					

ELEV.	DEPTH	S	T	N	L	R	DO	DESCRIPTION	10	20	30	40	50
									Wc ▲ NATURAL				

LEGEND: DEPTH—FEET BELOW GROUND SURFACE

S — SAMPLE NUMBER

T — TYPE OF SAMPLE

N — PENETRATION, BLOWS PER FOOT

L — SAMPLE LENGTH

R — LENGTH OF SAMPLE RECOVERED

DO — DRY DENSITY, LB. PER CU. FOOT

WO — WASHOUT

A — AUGER

HS — HOLLOW STEM AUGER

SS — SPLIT SPOON

ST — SHELBY TUBE

FT — FISH TAIL

C — CORE

Wc — WATER CONTENT PERCENT

BCR — BEFORE CASING REMOVAL

ACR — AFTER CASING REMOVAL

WD — WHILE DRILLING

WCI — WET CAVE IN

DCI — DRY CAVE IN

Qu — UNCONFINED COMPRESSIVE STRENGTH POUNDS PER SQUARE FOOT

FOR: Sexton Filling & Grading Corporation

SOIL BORING LOG NO. 9

PROJECT: 12100 West 31st Street

WALTER H. FLOOD & CO., INC.

LOCATION Westchester, Illinois

• **Engineers** •

METHOD OF BORING: HS

WATER LEVEL READINGS

SPLIT SPOON SIZE: 2 IN.

18.5' W.D.

WT. OF HAMMER 140 LBS.

19.0' B.C.R.

INCH DROP 30

17.2' A.C.R.

SHELBY TUBE SIZE

17.0'@24HRS. AFTER DRILLING

CASING USED 20'-2½" IDHS

HRS. AFTER DRILLING

DATE OF BORING: 3-29-72

RY: BJ&JA:bc

JOB NO.: 7205-0010

VERTICAL SCALE: 1"=10'

[illegible]

BEDROCK

FOR: Sexton Filling & Grading Corporation		SOIL BORING LOG NO. 10	
PROJECT: 12100 West 31st Street		WALTER H. FLOOD & CO., INC.	
LOCATION: Westchester, Illinois		• Engineers •	
METHOD OF BORING: HS		• CHICAGO • KALAMAZOO •	
SPLIT SPOON SIZE: 2 IN.		DATE OF BORING: 3-17-72	
WT. OF HAMMER 140 LBS.		BY: BJ&JA:bc	
INCH DROP 30		JOB NO.: 7205-0010	
SHELBY TUBE SIZE		VERTICAL SCALE: 1"=10'	
CASING USED 37'-2 1/4" IDHS			
WATER LEVEL READINGS			
6.0' W.D.			
21.7' B.C.R.			
20.5' A.C.R.			
5.7' @ 24 HRS. AFTER DRILLING			
HRS. AFTER DRILLING			

ELEV.	DEPTH	S	T	N	LF	DO	DESCRIPTION	Qu • LABORATORY X 1000	O PENETROMETER			
								2	4	6	8	10
656.5	0.0						Ground surface					
		1	ss	12			Fill, brown&black clay,wood			20.2		
		2	ss	20								
		3	ss	7						22.0		9000
648.0	8.5	4	ss	22			Brown and gray clay, trace of small gravel, hard to very tough					
		5	ss	12				3500				
		6	ss	12				2000		17.1		
		7	ss	12						18.8		
		8	ss	20								
635.5	21.0	9	ss	5 1/4"			Gray silt, some fine to coarse sand, small to large gravel, occasional boulder, very dense		12.3	4200		
		10	ss	100/2"					14.4			
630.5	26.0	11	ss	17			Gray clay, trace of small to large gravel, tough to very tough			3300		
		12	ss	21								
		13	ss	61								
623.0	33.5	14	ss	110			Gray silt, fine to coarse sand small to large gravel, boulders, stone fragments, very dense		13.1	5000		
619.5	37.0	15	ss	100/3"								
615.0	41.5	16	C				Light gray dolomite, thinly bedded, fractured, dense					
							End of boring					

ELEV.	DEPTH	S	T	N	LF	DO	DESCRIPTION	10	20	30	40	50
								10	20	30	40	50

Wc ▲ NATURAL

LEGEND: DEPTH—FEET BELOW GROUND SURFACE
 S — SAMPLE NUMBER
 T — TYPE OF SAMPLE
 N — PENETRATION, BLOWS PER FOOT
 LF — SAMPLE LENGTH
 R — LENGTH OF SAMPLE RECOVERED
 DO — DRY DENSITY, LB. PER CU. FOOT
 WO — WASHOUT
 A — AUGER
 HS — HOLLOW STEM AUGER
 SS — SPLIT SPOON
 ST — SHELBY TUBE
 FT — FISH TAIL
 C — CORE
 Wc — WATER CONTENT PERCENT
 BCR — BEFORE CASING REMOVAL
 ACR — AFTER CASING REMOVAL
 WD — WHILE DRILLING
 WCI — WET CAVE IN
 DCI — DRY CAVE IN
 Qu — UNCONFINED COMPRESSIVE STRENGTH POUNDS PER SQUARE FOOT

FOR: Sexton Filling & Grading Corporation

SOIL BORING LOG NO. 11

PROJECT: 12100 West 31st Street

WALTER H. FLOOD & CO., INC.

LOCATION Westchester, Illinois

• **Engineers** •

METHOD OF BORING: HS

WATER LEVEL READINGS

SPLIT SPOON SIZE: 2 IN.

13.5' W.D.

WT. OF HAMMER 140 LBS.

11.6' B.C.R.

INCH DROP 30

14.3' A.C.R.

SHELBY TUBE SIZE

12.5' @ 24 HRS. AFTER DRILLING

CASING USED 17'-2½" IDHS

HRS. AFTER DRILLING

DATE OF BORING: 6-14-72

BY: DL&BS:bc

JOB NO.: 7205-0010

**VERTICAL
SCALE:** 1"=10'.

[illegible]

LEGEND: DEPTH—FEET BELOW GROUND SURFACE
S —SAMPLE NUMBER
T —TYPE OF SAMPLE
N —PENETRATION, BLOWS PER FOOT
L —SAMPLE LENGTH
R —LENGTH OF SAMPLE RECOVERED
DO — DRY DENSITY, LB. PER CU. FOOT

WO	- WASHOUT	BCF
A	- AUGER	ACF
HS	- HOLLOW STEM AUGER	WD
SS	- SPLIT SPOON	WCI
ST	- SHELBY TUBE	DCI
FT	- FISH TAIL	Qu
C	- CORE	
Wc	- WATER CONTENT PERCENT	

BCR—BEFORE CASING REMOVAL
ACR—AFTER CASING REMOVAL
WD —WHILE DRILLING
WCI —WET CAVE IN
DCI — DRY CAVE IN
Qu — UNCONFINED COMPRESSIVE STRENGTH
POUNDS PER SQUARE FOOT

BEDECK

FOR: Sexton Filling & Grading Corporation PROJECT: 12100 West 31st Street LOCATION: Westchester, Illinois		SOIL BORING LOG NO. 13 WALTER H. FLOOD & CO., INC. • Engineers • • CHICAGO • KALAMAZOO •	
METHOD OF BORING: HS SPLIT SPOON SIZE: 2 IN. WT. OF HAMMER: 140 LBS. INCH DROP: 30 SHELBY TUBE SIZE: 22'-2 1/2" IDHS CASING USED: 22'-2 1/2" IDHS		WATER LEVEL READINGS 13.5' W.D. 10.8' B.C.R. 11.9' A.C.R. 12.2' @ 24 HRS. AFTER DRILLING HRS. AFTER DRILLING	
		DATE OF BORING: 6-14-72	BY: DL&BS:bc
		JOB NO.: 7205-0010	VERTICAL SCALE: 1"=10'

ELEV.	DEPTH	S	T	N	L	R	DD	DESCRIPTION	Qu • LABORATORY O PENETROMETER X 1000				
									2	4	6	8	10
651.2	0.0							Ground surface					
		1	ss	13				Gray clay, trace of small to large gravel, very tough		17.4▲		6000○	
		2	ss	11						18.2▲		5000○	
		3	ss	29						17.1▲		5000○	
643.7	7.5	4	ss	18				See note 1					
641.2	10.0	5	ss	7				Gray clayey silt, trace of small gravel					
638.7	12.5	6	ss	23				See note 2					
636.2	15.0	7	ss	26				Gray fine sand, trace of silt, medium dense					
633.7	17.5	8	ss	28				Gray silt, some fine to coarse sand, small to large gravel, boulders					
628.7	22.5	9	ss	10 5/8"									
		10	C					Light gray dolomite, thinly bedded, fractured, dense					
623.7	27.5							End of boring					
								Note 1: Gray medium sand, some silt, small to large gravel, boulders, medium dense					
								Note 2: Gray fine to medium sand, some silt, small to large gravel, medium dense					

LEGEND: DEPTH—FEET BELOW GROUND SURFACE
 S — SAMPLE NUMBER
 T — TYPE OF SAMPLE
 N — PENETRATION, BLOWS PER FOOT
 L — SAMPLE LENGTH
 R — LENGTH OF SAMPLE RECOVERED
 DD — DRY DENSITY, LB. PER CU. FOOT

WO — WASHOUT
 A — AUGER
 HS — HOLLOW STEM AUGER
 SS — SPLIT SPOON
 ST — SHELBY TUBE
 FT — FISH TAIL
 C — CORE
 Wc — WATER CONTENT PERCENT

BCR—BEFORE CASING REMOVAL
 ACR—AFTER CASING REMOVAL
 WD — WHILE DRILLING
 WCI — WET CAVE IN
 DCI — DRY CAVE IN
 Qu — UNCONFINED COMPRESSIVE STRENGTH
 POUNDS PER SQUARE FOOT

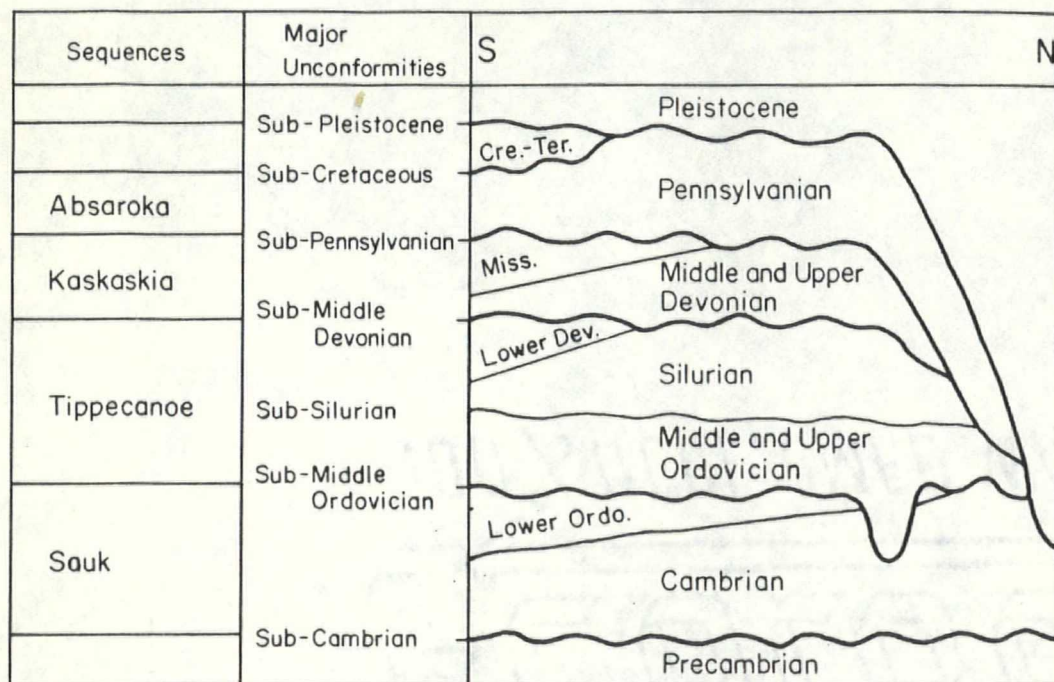


Fig. 6 - Diagrammatic cross section from southern to northern Illinois showing major unconformities and named sequences.

that the Henry Formation is Wisconsinan in age, but the Henry Formation is a rock-stratigraphic unit, not a subdivision of the Wisconsinan Stage. It is differentiated from other formations because of its composition and not because of its age.

STRATIGRAPHIC RELATIONS

Most of the stratigraphic units in the Chicago area have a conformable relation, that is, no significant interruptions in deposition took place. Even though the composition of the sediment changes at the contact between the units, deposition was essentially continuous. At many contacts, however, the lower unit was partly or completely eroded before the overlying sediment was deposited. Contacts where deposition was interrupted and beds are missing are unconformities.

Where the beds above and below an unconformity are essentially parallel, the unconformity is called a disconformity, and where the lower beds were tilted before overlying beds were deposited, the contact is called an angular unconformity. The contact between the Silurian and Ordovician rocks in the Chicago area is a disconformity, whereas the Silurian and Pennsylvanian rocks dip slightly in opposite directions and the contact between them is an angular unconformity.

Minor unconformities that are of limited extent and represent no great amount of erosion occur between some units, particularly the units differentiated in the glacial deposits. Sharp, undulating contacts between and within many units may be depositional features; they are not unconformities unless there is evidence that beds are missing.

The major unconformities, as previously noted, are used to differentiate units called sequences. A diagrammatic cross section from southern to northern Illinois (fig. 6) shows the stratigraphic relations of the sequences, although it distorts their thicknesses and dips. It reveals the major tectonic events (vertical or tilting movements) and the erosional events in the geologic history of the area. These events are summarized below:

The oldest and which were metamorphic earth. They were intrusive; later they were uplifted; the beginning of the Cambrian unconformity surface in the Chicago area are locally prominent (fig. 1).

Only a minor (Canadian) rocks that comprise the tectonic of the continent caused the basal middle Ordovician rocks in the lower parts of the area (the surface, locally characterizing the margin of the lower rocks are present again movement along the Kaskaskia Ottawa areas to the west).

The next youngest rocks, where it forms the and Lower Devonian widespread but minor (cinnatian) rocks, the indicates the middle Ordovician.

The end of Ordovician as 150 feet deep in the were filled with early evidence of unconformity and this unconformity Sequence. In Illinois Lower Devonian rocks apparently was continuous.

The sub-Middle is related to an interval a result of tilting and Devonian, the upper Silurian north of central Illinois strata completely the Chicago area the tion of the basal unconformity the region. Overlap on top of the Silurian Teeth of Devonian or (fig. 11B). Although the cago area, Upper Devonian in the fault blocks of either remained above Middle Devonian rock time. In either case Arch.